PremiumSoft Navicat Premium Enterprise V9.1.8 Keygen Serial [Kk Full Version where

$$\alpha = \frac{(w_1 + w_2) + \sqrt{(w_1 + w_2)^2 - 4c}}{2} \tag{6}$$

$$\beta = \frac{(w_1 + w_2) - \sqrt{(w_1 + w_2)^2 - 4c}}{2}. \tag{7}$$

Of course, the number of trees in graph G_n according to (2) and (5) will be

$$D_n = d\,\frac{\alpha^n - \beta^n}{\alpha - \beta}. \tag{8}$$

It is interesting to note that for a ladder graph, equation (3a) generates the even index terms of the sequence of Fibonacci numbers, which agrees with Bubnicki's result [9].

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n-Port Rectangular-Shaped Distributed RC Networks

I. INTRODUCTION

Being a model for the molecular electronic system, distributed RC (resistance capacitance) networks have drawn considerable attention during the last decade. Following others [1]–[7], Heizer [8]–[10] first pointed out that distributed systems can also be made to have rational short-circuit admittance parameters by choosing appropriate geometry of a two-port rectangular three-layer structure. Later, Barker [11] and Woo and Hove [12] applied his result to practical circuit realizations. Heizer introduced a condition for giving the rational functions but did not mention the uniqueness.

This correspondence, using a different but simpler derivation, furnishes a necessary and sufficient condition for generating rational functions of that structure. Furthermore, it is generalized to n-port structures. While the formulation may seem deceptively simple, it does present a unified and comprehensive analysis of the various network properties which are indispensable to the synthesis problem. In the limiting case, the resulting solution can also provide an insight into the transcendental network functions.

II. THE BASIC DIFFERENTIAL EQUATION

Consider the network representation of an elementary length, Δx, of a layer structure with both normalized dimensions and coordinates (Fig. 1). $C_a(x)$ and $C_b(x)$ are the capacitance per unit length in the x-direction between the resistive film and the lower and the upper conductors, respectively. The resistive film has a resistance R per unit length in the x-direction, but no resistance in the y-direction.[1] $J_a(x)$ and $J_b(x)$ are currents per unit length, directed in the z-direction. $I_0(x)$ is the current in the resistive film in the x-direction. $v(x)$ is the voltage across the capacitance $C_a(x)$. Further, we assume that the wavelength in the dielectric is much longer than the dimensions of the structure. Then,

$$v(x) - I_0(x)R\Delta x - v(x + \Delta x) = 0 \tag{1}$$

and

$$sC_a(x)\Delta x\, v(x) + I_0(x) - sC_b(x)\Delta x\{V - v(x)\} - I_0(x - \Delta x) = 0. \tag{2}$$

Eliminate $I_0(x)$ from (1) and (2) to give

$$-\frac{v(x + \Delta x) - 2v(x) + v(x - \Delta x)}{(\Delta x)^2} + s[C_a(x) + C_b(x)]Rv(x) - sC_b(x)RV = 0. \tag{3}$$

If the second derivative of $v(x)$ exists, the difference equation becomes the following second-order linear differential equation as $\Delta x \to 0$,

$$\frac{d^2v(x)}{dx^2} - sR\{C_a(x) + C_b(x)\}v(x) = -sC_b(x)RV. \tag{4}$$

Equation (4), an analogy of the telegraph equation of the transmission lines, is considered as the differential equation for the structure shown in Fig. 2.

III. RECTANGULAR LAYER STRUCTURES

In Fig. 3, a distributed circuit is illustrated. The resistive film has R ohms per unit length in the x-direction, and no resistance in the y-direction. The total capacitance due to the dielectric between the resistive film and the conductors in the x-direction per unit length is C farads. The conductor is cut into $(n + 1)$ pieces (Fig. 3); the voltage at conductor 0 is the reference. The capacitance between the film and the conductor k is $C_k(x)$, $k = 0, 1, \cdots, n$. Thus, this structure is actually an n port network (Fig. 4). The short-circuit parameters can be obtained as follows.

a)

$$y_{ii} = \left.\frac{I_i}{V_i}\right|_{V_k = 0} \qquad k = 1, 2, \cdots, n; \qquad k \neq i. \tag{5}$$

Let

$$C_a(x) = C - C_i(x), \qquad C_b(x) = C_i(x)$$
$$\gamma^2 = sRC, \qquad C_i(x) = Cf_i(x), \qquad V = V_i$$

be substituted into (4):

$$\frac{d^2v(x)}{dx^2} - \gamma^2 v(x) = -\gamma^2 f_i(x) V_i. \tag{6}$$

The general solution of (6) is

$$v(x) = Ae^{\gamma x} + Be^{-\gamma x} + V_i g_i(\gamma, x), \tag{7}$$

where $g_i(\gamma, x) = (1 - D^2/\gamma^2)^{-1} f_i(x)$ is not an algebraic equation; its right side expresses the operation of $(1 - D^2/\gamma^2)^{-1}$ on the function $f_i(x)$ with $D = d/dx$. A and B can be determined from the two boundary conditions,

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[1] This assumption can be realized approximately by making many conducting stripes parallel to the y-axis on the resistive film. However, by using uniform resistive film instead, Barker [11] and Woo and Hove [12] obtained experimental results which agree fairly close to the theoretical calculations under this assumption.

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